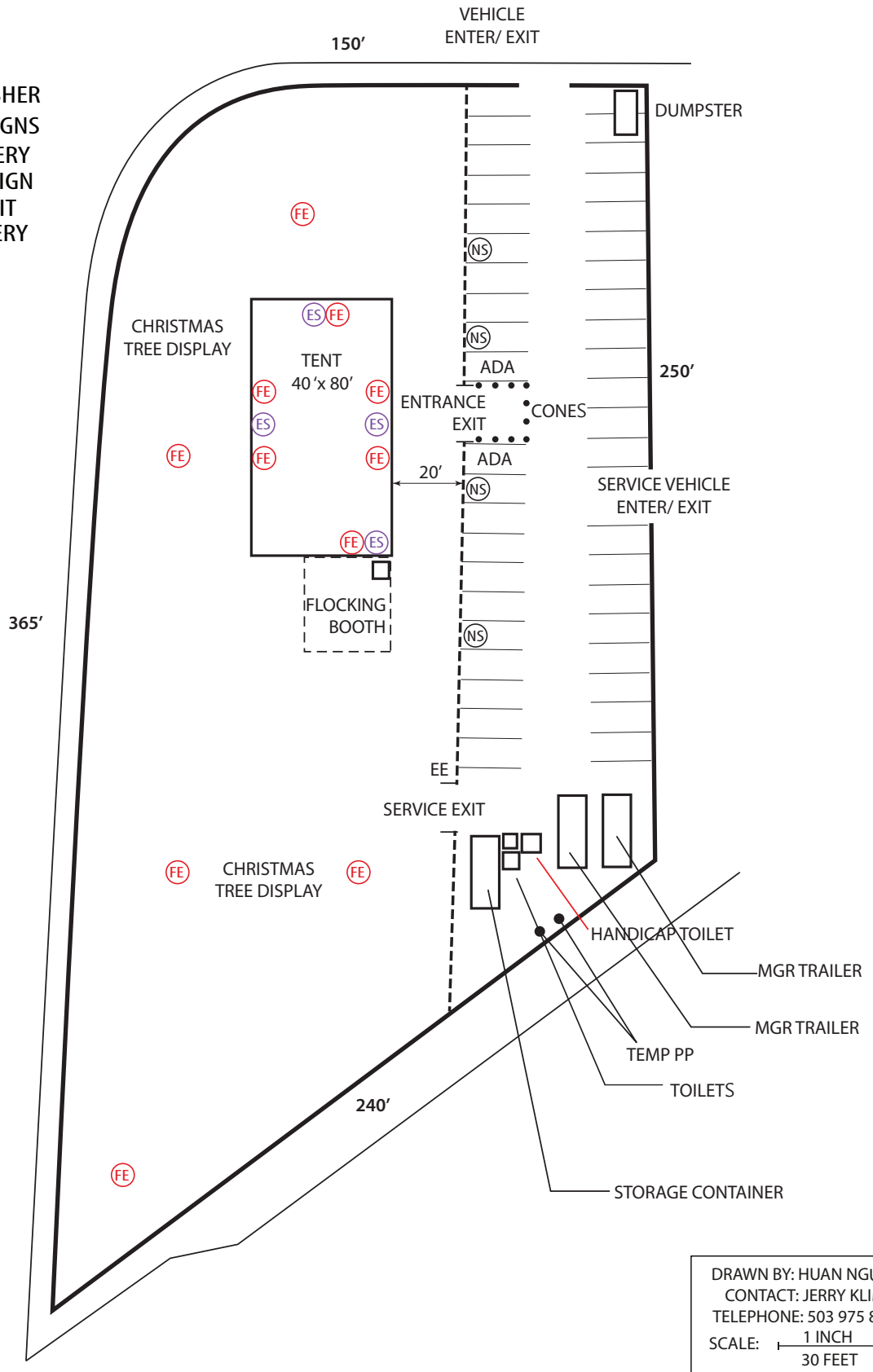


# ABC TREE FARMS CHRISTMAS TREES 3590 BENTON STREET APN 290-22-154

## BENTON STREET

- ⓕ = FIRE EXTINGUISHER
- Ⓝ = NO SMOKING SIGNS
- ⓔ = LIGHT UP BATTERY BACK UP EXIT SIGN
- EE = EMERGENCY EXIT LIGHT UP BATTERY BACK UP

## LAWRENCE EXPRESSWAY



DRAWN BY: HUAN NGUYEN  
CONTACT: JERRY KLIMA  
TELEPHONE: 503 975 8733  
SCALE: 1 INCH = 30 FEET



DESIGN & DEVELOPMENT

CIVIL ENGINEERING – STRUCTURAL ENGINEERING – MECHANICAL ENGINEERING – ELECTRICAL ENGINEERING

425 Virginia Street Suite B, Vallejo CA 94590

Main Tel: 707-648-9571

[www.monarchengineers.com](http://www.monarchengineers.com)

## STAKING CALCULATIONS 40'x80' TENT

FOR

ABC TREE FRAMS, LLC

Project Location: 3590 Benton Street  
Santa Clara, California

JOB No. 23-001SCR  
DATE: May 19, 2023



MONARCH ENGINEERING WAS ENGAGED TO PROVIDE CALCULATIONS AND CONSULTATION IN CONNECTION WITH THE ABOVE DESCRIBED PROJECT. WE HAVE NO AUTHORITY INSOFAR AS CONTRACTOR'S OR OWNER'S PERSONNEL ARE CONCERNED. OWNER AND CONTRACTOR ARE OBLIGATED TO OBSERVE ALL SAFETY ORDINANCES FOR PROTECTION OR PERSONNEL. IN MAKING USE OF THESE DOCUMENTS, CONTRACTOR/OWNER AGRESS TO HOLD MOANARCH ENGINEERING HARMLESS FROM ALL COSTS OF LITIGATION THAT MAY ARISE OUT OF ALLEGED DAMAGES OR INJURIES ASSOCIATED WITH THE WORK DEFINED BY THESE DOCUMENTS, INCLUDING ATTORNEY'S FEES AND JUDGEMENTS, UNLESS IT IS PROVEN THAT SAID INJURIES OR DAMAGES RESULTED FROM ERRORS IN OR OMISSIONS FROM THE DOCUMENTS. MONARCH ENGINEERING DOES NOT PROVIDE GEOTECHNICAL SERVICES, ANY ISSUES RELATING TO SOILS MUST BE REVIEWED BY A GEOTECHNICAL ENGINEER.

This report shows the anchoring requirements for the tent size mentioned on the cover letter. The tent will be in place for less than 180 days so the temporary wind load reduction applies to the calculation criteria per CBC 2022 and ASCE 7-22. This tent will be installed on the existing asphalt parking lot. In The temporary-structure environment one underlying assumption is that the temporary structure is designed and manufactured under a particular building code in effect at the time the structure is manufactured. An unmodified structure is equivalent to an existing building in the sense that an existing building is not re-engineered every time a new code goes into effect. Therefore, the actual structural design of each member is not analyzed every time the structure is installed. A site-specific wind load analysis is done to determine anchoring, or ballasting required for a particular installation. To minimize the risk a high wind management plan is added to this report and is expected that the installer will follow the protocols outlined in the high wind management plan.

High wind management plan has been included in this package to be implemented, as part of this installation. This management plan serves as minimum requirements.



## **OPERATIONS MANAGEMENT PLAN**

### **IMPLEMENTATION OF PLAN**

1. PRIOR TO EACH INSTALLATION, LANTIER TENT SHALL DESIGNATE A RESPONSIBLE PERSON IN CHARGE OF IMPLEMENTING ALL PHASES OF THE OPERATIONS MANAGEMENT PLAN.
2. A MEETING SHALL BE HELD AT THE VENUE WITH THE PROMOTER, OWNER OR STAGE MANAGER TO DISCUSS THE HIGH WIND ACTION PLAN AND OTHER OPERATIONAL ITEMS.
3. THE METHOD OF INITIATING EVENT CANCELLATION OR TENT EVACUATION MUST BE OUTLINED EXPLICITLY PRIOR TO THE EVENT ALLOWING FOR IMMEDIATE ACTION IF NECESSARY.
4. A COPY OF THIS PLAN SHOULD BE PROVIDED TO LOCAL POLICE OR FIRE DEPARTMENTS IN ORDER TO HELP USHER PATRONS IN THE EVENT OF AN EVACUATION.

### **DAILY OPERATIONS PLAN**

1. CHECK WEATHER EACH MORNING AND PERIODICALLY THROUGHOUT THE DAY.
2. CHECK TENT BASES AND BALLAST DAILY TO ENSURE ALL REMAIN LEVEL AND PLUMB.
3. CHECK GUY WIRES/STRAPS AND/OR BALLAST ASSEMBLIES DAILY TO VERIFY LINES ARE TENSIONED AND BALLAST HAS NOT MOVED.
4. PROVIDE A DAILY LOG OF THE ABOVE CHECKS FOR EACH INSTALLATION.

### **HIGH WIND ACTION PLAN**

1. THE HIGH WIND ACTION PLAN SHALL BE IN EFFECT FOR THE ENTIRETY OF THE EVENT. AN EVENT SHALL BE DEFINED AS STARTING AT THE INITIAL COMMENCEMENT OF THE STRUCTURE INSTALLATION AND ENDING ONCE THE STRUCTURE IS COMPLETELY DISMANTLED.
2. A COMPETENT RESPONSIBLE PERSON FROM THE VENUE OR INSTALLER SHALL BE PRESENT FOR THE DURATION OF THE EVENT TO IMPLEMENT THE HIGH WIND ACTION PLAN (SEE ABOVE).
3. A REGULAR LIAISON WITH LOCAL AIRPORTS AND/OR WEATHER INFORMATION CENTERS SHALL BE MAINTAINED TO ASCERTAIN IF ANY SIGNIFICANT WEATHER EVENTS ARE EXPECTED IN THE IMMEDIATE VICINITY OF THE STRUCTURE.
4. AN ANEMOMETER SHALL BE PLACED ON THE STRUCTURE TO MONITOR WIND SPEEDS. THE ANEMOMETER SHALL BE PLACED AT THE TOP OF A TOWER OR AN ADJACENT STRUCTURE AT A HEIGHT EQUIVALENT TO THE HEIGHT OF THE MEAN HEIGHT OF THE ROOF TENT. THE ANEMOMETER SHALL BE LOCATED WITHIN 50 YARDS OF THE STRUCTURE.



5. NOTED WIND SPEEDS ARE 3-SECOND GUSTS IN ACCORDANCE WITH ASCE 7
  6. **WHEN THE STRUCTURE IS UNATTENDED OR NOT IN USE:** ALL DOORS OR OPENINGS SHALL BE KEPT CLOSED.
  7. **WHEN WIND SPEEDS ARE EXPECTED TO EXCEED 30 MPH:** A TEAM OF QUALIFIED PERSONNEL SHALL BE PUT ON ALERT. ALL NECESSARY PERSONNEL SHALL BE IN PLACE AND PUT ON STANDBY.
  8. **WHEN WIND SPEEDS REACH 30 MPH:** A TEAM OF QUALIFIED PERSONNEL SHALL START INSPECTING BALLAST SYSTEM TO MAKE SURE ALL ELEMENTS ARE IN PLACE AND SET UP EVACUATION PLAN.
  9. **AT WINDS SPEEDS IN EXCESS OF 45 MPH:** A TEAM OF QUALIFIED PERSONNEL SHALL START EVACUATION PLAN. VERIFY THAT BALLAST SYSTEM ARE IN PLACE AND NOT MOVING.
  10. THE HIGH WIND ACTION PLAN SHALL BE POSTED AT A CONSPICUOUS AREA ON SITE. IT MUST BE AVAILABLE AT ALL TIMES TO VENUE OPERATORS AND CREW.
-

Staking Guide 2014 published by the Industrial Fabrics Association International

Soil Consistency	Pullout Capacity (lbs)
Hard (very dense)	2,500
Very Stiff (Dense)	1,600
Stiff (Medium dense)	<b>800</b>
Medium (Medium)	400
Soft (Loose)	200
Very Soft (Very loose)	100

The capacities listed are for the following conditions:

- 1) 36" minimum embedment
- 2) 1" diameter steel stake
- 3) stakes angle 0 to 15 degrees
- 4) Fastening height 2" or less
- 5) Load angle 45 degrees

Group Configuration	Effectiveness Factor
Double Staking	1.22

Three stakes installed in a line perpendicular to direction of pull	2.76
---	------

Three stakes installed in a line perpendicular to direction of pull are inclined at 15 degrees	2.46
--	------

Six stakes installed in a line perpendicular to direction of pull	4.68
---	------

Four stakes installed in two columns and two rows and connected with a gang plate	3.48
---	------

Six stakes installed in two columns and three rows and connected with a gang plate	4.56
--	------

P = Pullout Capacity for a single stake

$$P = P_b \times C_e \times C_f \times C_i \times C_l \times C_d < 2,500\#$$

$P_b$	Pullout capacity for standard stake
$C_e$	Correction factor for embedment depth
$C_f$	Correction factor for stake fastening height
$C_i$	Correction factor for stake inclination
$C_l$	Correction factor for load angle
$C_d$	Correction factor for stake diameter

1" diameter steel stake

$P_b$ (lbs.)	800
$C_e$	1
$C_f$	1
$C_i$	1
$C_l$	1
$C_d$	1
$P$ (lbs)	800



# MONARCH ENGINEERS

MONARCH ENGINEERS  
425 Virginia Street, Ste. B, Vallejo CA 94590  
Tel: 415-448-6073 - Tel: 707-648-9571

This calculation package is only valid for the tent size specified in the "Tent Size" field below. The use of these type of structure is temporary in nature; therefore this package is only valid for structures that will remain in place for less than 180 days. Any period of time exceeding 180 days is not considered temporary according to the current building code. This package only determines the required ballast system necessary for safe application. Structural design of the actual structure had been done by others at the time when the structure was built. We are assuming no modification or alterations have been done to the structure since it was manufactured; therefore we treat this structure as an existing building for internal connection purposes not required to be brought up to current code every time it is erected.

We have analyzed the ballast system requirements based on ASCE 7-22.

## Tent Size

40'x80'x7.67' Exposure B

Temporary structures are erected and occupied for periods of 180 days or less, this is equivalent to an 10-year MRI. Therefore the expected risk to experience winds that a permanent structure will experience is its lifetime is much lower. In addition, this installation comes with a high wind management plan to further reduce the risk of catastrophic failure. Based on this allowance we calculate the potential wind load to be based on 10-year MRI

## WIND CRITERIA

Occupancy Category:	II
Basic Wind Speed , V:	64 mph ASCE 7-22
Wind Exposure:	B

TENT PROPERTIES

Span, L (ft): 40.00  
 Roof Height, H (ft): 18.00  
 Mean Roof Height, h (ft): 13.00  
 Roof Slope (degrees): 27.00  
 Bay Width (ft): 10.00  
 Length, B (ft): 80.00  
 Leg Height, z (ft): 7.67  
 Roof Rafter Length, (ft) 22.36  
 Number of Bays 8  
 Number of Legs @ Gable End 5

Roof Equip. Load = 1.25 psf  
 Roof DL = 1.25 psf

Adj. (0.6)  
 0.75 psf  
 0.75 psf

Wind Calculations

$q_z = 0.00256K_zK_dV$

$V = 64.00$  mph

$K_{zt} = 1.00$  ASCE 7-22 Section 26.8.2  
 $K_z = 0.70$  ASCE 7-22 Table 26.10-1  
 $K_d = 0.85$  ASCE 7-22 Table 26.6-1  
 $K_e = 1.00$  ASCE 7-22 Table 26.9-1

Enclosure Classification = Enclosed

$GC_{pi} = 0.18$  ASCE 7-22 Table 26.13-1  
 $-0.18$

$q_z = 6.24$  psf

LOAD CASE A

BUILDING SURFACE								
$\theta$ (°)	1	2	3	4	1E	2E	3E	4E
27	0.55	-0.06	-0.45	-0.39	0.72	-0.13	-0.58	-0.53

LOAD CASE B

BUILDING SURFACE												
$\theta$ (°)	1	2	3	4	5	6	1E	2E	3E	4E	5E	6E
27	-0.45	-0.69	-0.37	-0.45	0.40	-0.29	-0.48	-1.07	-0.53	-0.48	0.61	-0.43

LOAD CALCULATIONS

LOAD CASE A

WIND PRESSURE q (psf)								
BUILDING SURFACE								
CASE	1	2	3	4	1E	2E	3E	4E
GC <sub>pi</sub>	2.31	-1.50	-3.93	-3.56	3.37	-1.93	-4.74	-4.43
-GC <sub>pi</sub>	4.55	0.75	-1.68	-1.31	5.62	0.31	-2.50	-2.18

LOAD CASE B

WIND PRESSURE q (psf)												
BUILDING SURFACES												
CASE	1	2	3	4	5	6	1E	2E	3E	4E	5E	6E
GC <sub>pi</sub>	-3.93	-5.43	-3.43	-3.93	1.37	-2.93	-4.12	-7.80	-4.43	-4.12	2.68	-3.81
-GC <sub>pi</sub>	-1.68	-3.18	-1.19	-1.68	3.62	-0.69	-1.87	-5.55	-2.18	-1.87	4.93	-1.56

a= 4.00

LOAD CASE A

AREAS (ft <sup>2</sup> )						
BUILDING SURFACE						
1	2	3	4	1E	2E	3E
552	1,610	1,610	552	61	179	179
					4E	61

LOAD CASE B

AREAS (ft <sup>2</sup> )						
BUILDING SURFACES						
1	2	3	4	5	6	1E
552	1,610	1,610	552	730	730	61
					2E	179
					3E	179
					4E	61
					5E	4
					6E	4

LOAD CASE A

FORCE (lbs)						
BUILDING SURFACE						
CASE	1	2	3	4	1E	2E
GCpi	1,274	-2,411	-6,328	-1,963	207	-346
-GCpi	2,514	1,205	-2,712	-723	344	56
					3E	-848
					4E	-272
						-134

LOAD CASE B

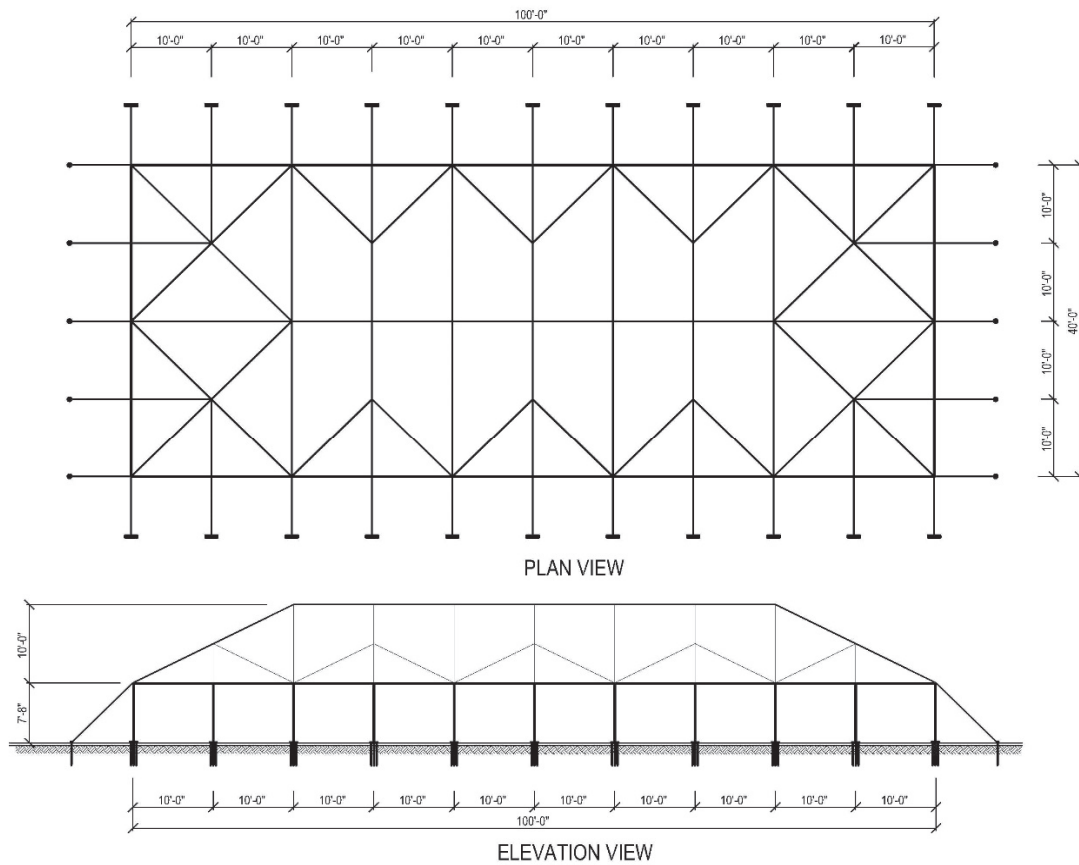
FORCE (lbs)						
BUILDING SURFACES						
CASE	1	2	3	4	5	6
GCpi	-2,170	-8,739	-5,525	-2,170	1,002	-2,140
-GCpi	-930	-5,123	-1,908	-930	2,641	-501
					1E	-253
					2E	-1,395
					3E	-792
					4E	-253
					5E	12
					6E	-17
						-7

LOAD CASE A

FORCE (lbs)							
BUILDING SURFACE							
1	2	3	4	1E	2E	3E	4E
2,514	-2,411	-6,328	-1,963	344	-346	-848	-272

LOAD CASE B

FORCE (lbs)											
BUILDING SURFACES											
1	2	3	4	5	6	1E	2E	3E	4E	5E	6E
-2,170	-8,739	-5,525	-2,170	2,641	-2,140	-253	-1,395	-792	-253	22	-17



2a = 8.00 ft

Grid lines 1 & 9

Shear Force,  $F_s$  (#)

q (psf) 5.62

Area (ft<sup>2</sup>) 31

$F_s$ (#)	172	0	172
-----------	-----	---	-----

Uplift Force,  $F_u$  (#)

q (psf) -7.80 D.L. 0.75

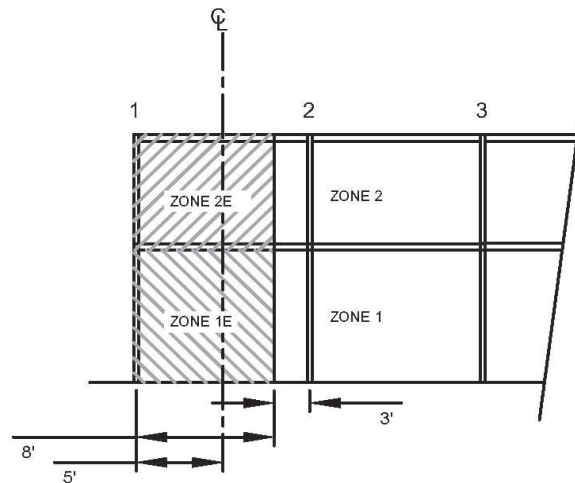
Area (ft<sup>2</sup>) 89 Total

$F_u$ (#)	-563	0	-496
-----------	------	---	------

Resultant Force

$$F_R = \sqrt{F_s^2 + F_u^2}$$

$F_R$ (#)	525
-----------	-----



(1) One stake = 800 > 525 OK to use one stake

Grid lines 2 & 8

Shear Force,  $F_s$  (#)

q (psf)	5.62	4.55	4.55	
Area (ft <sup>2</sup> )	23	15	38	Total
$F_s$ (#)	129	70	175	374

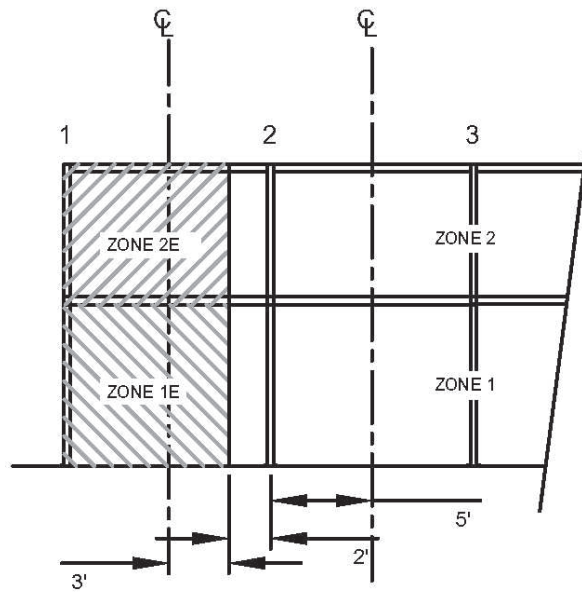
Uplift Force,  $F_u$  (#)

				D.L.
q (psf)	-7.80	-5.43	-5.43	0.75
Area (ft <sup>2</sup> )	67	45	112	Total
$F_u$ (#)	-423	-176	-439	-870

Resultant Force

$F_R = \sqrt{F_s^2 + F_u^2}$   
 $F_R$  (#) 795

(2) Two stakes = 976 > 795 OK to use two stakes



Grid lines 3 & 7

Shear Force,  $F_s$  (#)

q (psf)	4.55			
Area (ft <sup>2</sup> )	77			Total
$F_s$ (#)	349	0	0	349

Uplift Force,  $F_u$  (#)

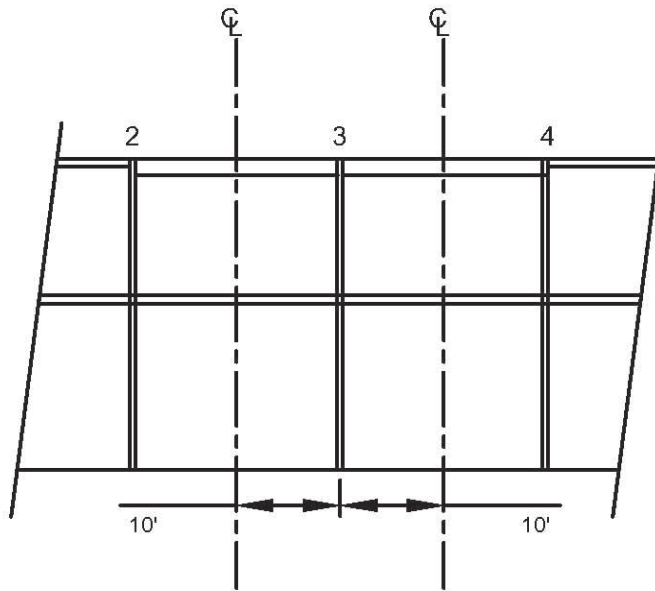
q (psf)	-1.50			D.L.
Area (ft <sup>2</sup> )	224			Total
$F_u$ (#)	-335	0	0	-167

Resultant Force

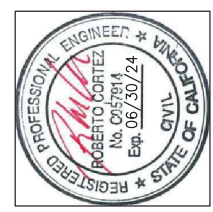
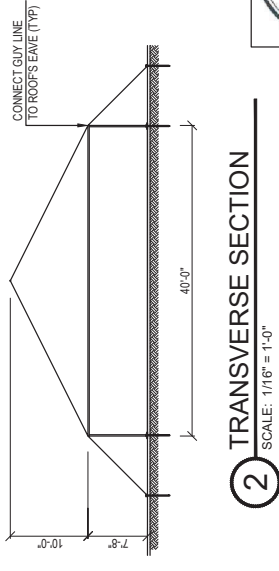
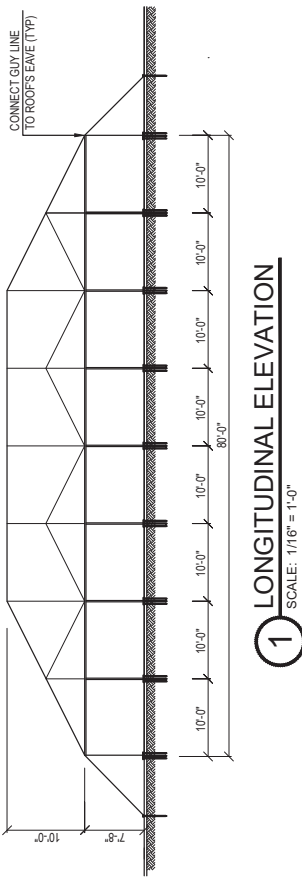
$$F_R = \sqrt{F_s^2 + F_u^2}$$

$F_R$  (#) 349

(1) One stake = 800 > 349 OK to use one stake



LEGEND	
●	SINGLE STAKE
—	STAKE BAR W/ 3 STAKES
TOTAL NUMBER OF SINGLE-STAKE ANCHORS = 10	
TOTAL NUMBER OF GROUP-STAKE ANCHORS = 22	

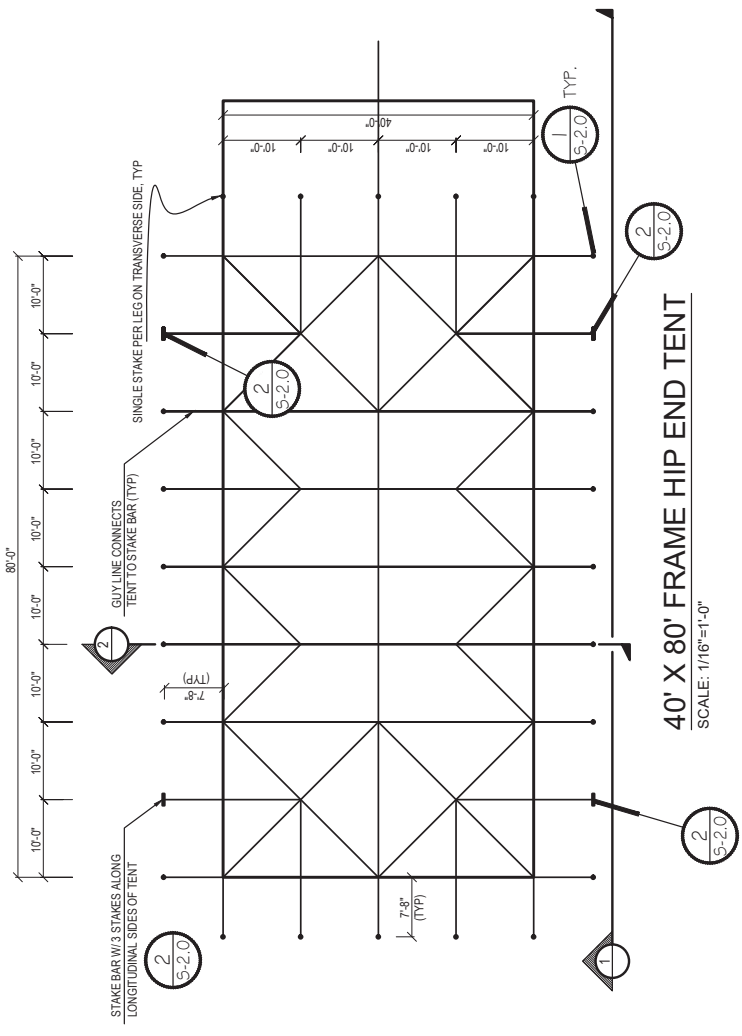


40' X 80' FRAME HIP END TENT  
 ABC TREE FARMS  
 3590 BENTON ST.  
 SANTA CLARA, CA

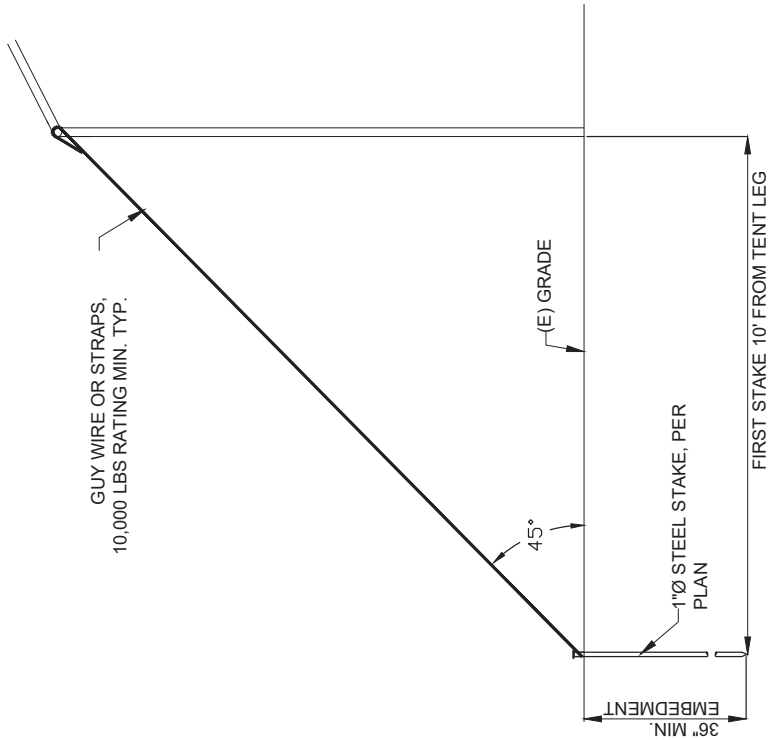
**MONARCH ENGINEERS**  
 ENERGY CONSERVATION, SUSTAINABILITY  
 STRUCTURAL ENGINEERING  
 CIVIL ENGINEERING  
 ELECTRICAL ENGINEERING  
 MECHANICAL ENGINEERING  
 DESIGN & DEVELOPMENT

425 Wright Street, Ste. B.  
 Menlo Park, CA 94025  
 TEL (415) 448-6073  
 TEL (707) 648-9571

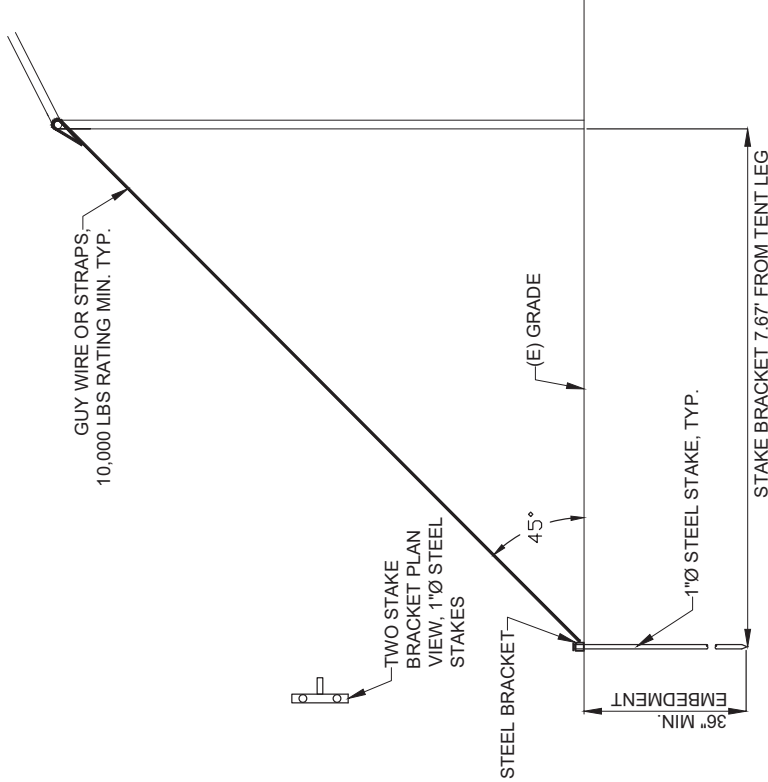
SIZE	DWG BY:	DESIGNED BY:	APPROVED BY:	REV
	Katy Perry	R. Cortez, PE	R. Cortez, PE	
SCALE: AS NOTED			05/19/2023	SHEET: S-1.0



REVISION HISTORY		
No.	DATE	DESCRIPTION
1	-	-
2	-	-
3	-	-



1 SINGLE STAKE DETAIL  
SCALE: NTS



2 TWO STAKE DETAIL  
SCALE: NTS

REVISION HISTORY

No.	DATE	DESCRIPTION
△	-	-
△	-	-
△	-	-



**MONARCH ENGINEERS**  
ENERGY CONSERVATION, SUSTAINABILITY  
STRUCTURAL ENGINEERING  
ELECTRICAL ENGINEERING  
MECHANICAL ENGINEERING  
DESIGN & DEVELOPMENT

425 Wright Street, Ste. B.  
Merced, CA 95341, CA  
TEL (415) 448-6073  
TEL (707) 648-9571

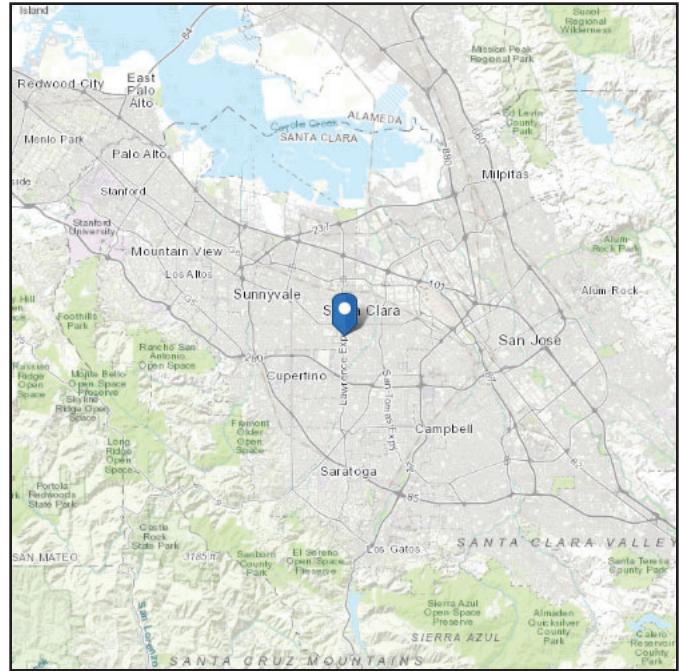
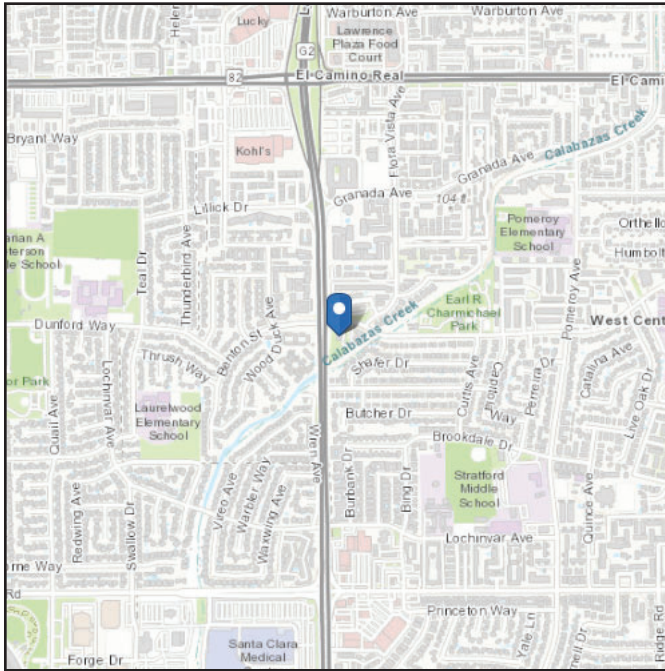
40' X 80' FRAME HIP END TENT ABC TREE FARMS 3590 BENTON ST. SANTA CLARA, CA		DESIGNED BY: R. Cortez, PE	APPROVED BY: R. Cortez, PE	REV
SIZE	DWG BY: Katy Perry	SCALE: AS NOTED	05/19/2023	REV
SHEET: S-2.0				

# ASCE 7 Hazards Report

**Address:**  
3590 Benton St  
Santa Clara, California  
95051

**Standard:** ASCE/SEI 7-22  
**Risk Category:** II  
**Soil Class:** Default

**Latitude:** 37.345026  
**Longitude:** -121.995206  
**Elevation:** 118.92212725038983 ft (NAVD 88)



## Wind

### Results:

Wind Speed	92 Vmph
10-year MRI	64 Vmph
25-year MRI	70 Vmph
50-year MRI	74 Vmph
100-year MRI	79 Vmph
300-year MRI	87 Vmph
700-year MRI	92 Vmph
1,700-year MRI	99 Vmph
3,000-year MRI	103 Vmph
10,000-year MRI	112 Vmph
100,000-year MRI	129 Vmph
1,000,000-year MRI	147 Vmph

Data Source: ASCE/SEI 7-22, Fig. 26.5-1B and Figs. CC.2-1-CC.2-4, and Section 26.5.2  
Date Accessed: Fri May 19 2023



Value provided is 3-second gust wind speeds at 33 ft above ground for Exposure C Category, based on linear interpolation between contours. Wind speeds are interpolated in accordance with the 7-22 Standard. Wind speeds correspond to approximately a 7% probability of exceedance in 50 years (annual exceedance probability = 0.00143, MRI = 700 years). Values for 10-year MRI, 25-year MRI, 50-year MRI and 100-year MRI are Service Level wind speeds, all other wind speeds are Ultimate wind speeds.

Site is not in a hurricane-prone region as defined in ASCE/SEI 7-22 Section 26.2.

The ASCE 7 Hazard Tool is provided for your convenience, for informational purposes only, and is provided “as is” and without warranties of any kind. The location data included herein has been obtained from information developed, produced, and maintained by third party providers; or has been extrapolated from maps incorporated in the ASCE 7 standard. While ASCE has made every effort to use data obtained from reliable sources or methodologies, ASCE does not make any representations or warranties as to the accuracy, completeness, reliability, currency, or quality of any data provided herein. Any third-party links provided by this Tool should not be construed as an endorsement, affiliation, relationship, or sponsorship of such third-party content by or from ASCE.

ASCE does not intend, nor should anyone interpret, the results provided by this Tool to replace the sound judgment of a competent professional, having knowledge and experience in the appropriate field(s) of practice, nor to substitute for the standard of care required of such professionals in interpreting and applying the contents of this Tool or the ASCE 7 standard.

In using this Tool, you expressly assume all risks associated with your use. Under no circumstances shall ASCE or its officers, directors, employees, members, affiliates, or agents be liable to you or any other person for any direct, indirect, special, incidental, or consequential damages arising from or related to your use of, or reliance on, the Tool or any information obtained therein. To the fullest extent permitted by law, you agree to release and hold harmless ASCE from any and all liability of any nature arising out of or resulting from any use of data provided by the ASCE 7 Hazard Tool.

# Certificate of Flame Resistance

REGISTERED  
APPLICATION  
CONCERN NO.

CAL COMB F-419.01

AZTEC TENTS  
490 ALASKA AVENUE  
TORRANCE, CA 90503  
(800)228-3687

Date treated or  
manufactured

12/2006

This is to certify that the materials described below hereof have been flame retardant treated (or are inherently nonflammable).

FOR

A-1 EQUIPMENT AND PARTY RENTAL  
ATTN: ROBBIE CRUIKSJANK  
831 EAST AVENUE R  
PALMDALE, CA 93550



Certification is hereby made that: (check "a" or "b")

- (a) The articles described below this certificate have been treated with a flame retardant chemical approved and registered by the State Fire Marshal and that the application of said chemical was done in conformance with the laws of the State of California and the Rules and Regulations of the State Fire Marshal.  
Name of chemical used ..... Chem. Reg. No. ....  
Method of application .....

- (b) The articles described below hereof are made from a flame -resistant fabric or material registered and approved by the State Fire Marshal for such use; Fabric has been tested and passes NFPA701-96.  
Trade name of flame-resistant fabric or material used.. *Laminated Fabric* ..... Reg. No. .... *F-419.01* .....

The Flame Retardant Process Used WILL NOT Be Removed by Washing  
(will or will not)

David Bradley

Name of Applicator or Production Superintendent

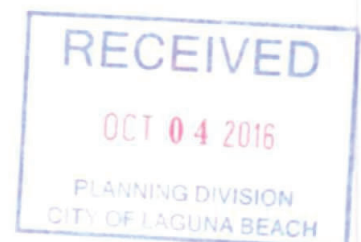
Chuck Miller - President

Title

CUSTOMER ORDER NO. R163630

## ITEMS MANUFACTURED:

- 1- 40'x40' (2 PC.) JUMBOTRAC TOP ONLY- ULTRA WHITE
- 1- 40'x10' JUMBOTRAC MIDDLE TOP ONLY- ULTRA WHITE
- 5- 40'x20' JUMBOTRAC MIDDLE TOP ONLY- ULTRA WHITE
- 2- 8'x10' JUMBOTRAC ACCESS SOLID WALL- ULTRA WHITE
- 16- 8'x10' JUMBOTRAC ACCESS SOLID WALL- ULTRA WHITE





# Certificate of Flame Resistance

Registered  
Application  
Number

F 4 1 9 . 0 1



I S S U E D B Y

Central Tent  
Santa Clarita, CA

Date of Manufacture:

12/5/14

**This is to certify that the materials described have been flame retardant treated (or are inherently nonflammable).**

F O R ABC Tree Farms, LLC

A D D R E S S PMB 367 - 25 NW 23rd Pl., Ste 6

C I T Y Portland

S T A T E OR

Z I P 97210

## Certification is hereby made that:

The articles described on this certificate have been treated with a flame-retardant fabric or material registered and approved by the State of California Fire Marshal. The article meets the NFPA-701 Flame retardant standard.

**Trade name of flame-resistant fabric or material used: Lam-Tex Reg. F419.01**

**The Flame Retardant Process Used will not be Removed by Washing.**

Type, Color, and weight of canvas / vinyl: White, Vinyl, 15oz

Description: (2) - 20x20 Complete Q-Peak, D-Tube, White Blackout, 15oz

Name of Applicator of Flame Resistant Finish:

California Combining Corporation

S I G N A T U R E

CENTRAL TENT MANUFACTURER